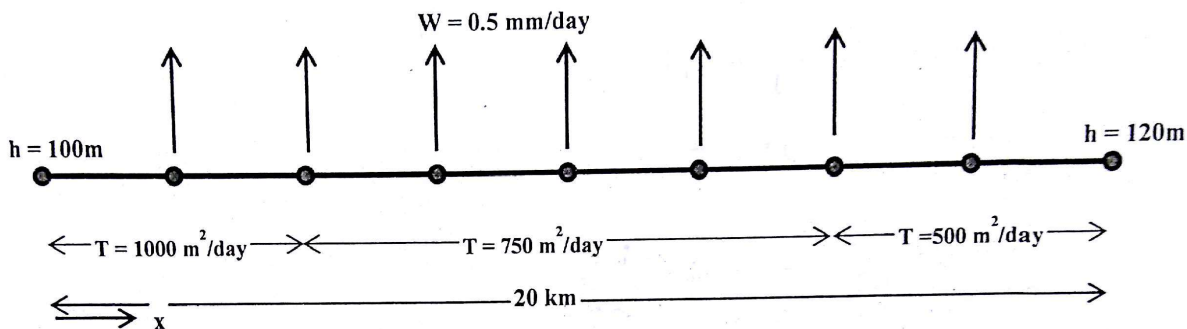


Anish Jaiswal

TUTORIAL - 5

Q1. A confined aquifer being considered in 1D is given. 20 km length of the aquifer is divided into 9 nodes equally spaced at 2.5 km. Boundary nodes have constant heads, 100 m on the first node and 120 m on the last node. All the interior nodes are subjected to uniform abstraction of 0.5 mm/day. Transmissivity between the first two intervals is 1000 m<sup>2</sup>/day, in next four intervals is 750 m<sup>2</sup>/day and in the last two intervals, it is 500 m<sup>2</sup>/day.

a) Compute steady state nodal heads by solving the appropriate differential equation numerically.



b) Assuming uniform transmissivity,  $T = 750 \text{ m}^2/\text{day}$ , on all the nodes, compute the steady state nodal heads by analytical method. Compare the results obtained in (a) and (b) and sketch the head distribution along x axis.

**THOMAS TRI-DIAGONAL MATRIX SOLUTION ALGORITHM**

It is a simplified form of Gaussian elimination that can be used to solve tri-diagonal systems of equations. A Tri-diagonal system for n unknowns may be written as

$$a_i x_{i-1} + b_i x_i + c_i x_{i+1} = d_i \quad i = 0, 2, \dots, n$$

$$\begin{bmatrix} b_0 & c_0 & & & 0 \\ a_1 & b_1 & c_1 & & \\ & a_2 & b_2 & c_2 & \\ & & \ddots & \ddots & \ddots \\ 0 & & & a_n & b_n \end{bmatrix} \begin{bmatrix} x_0 \\ x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix} = \begin{bmatrix} d_0 \\ d_1 \\ d_2 \\ \vdots \\ d_n \end{bmatrix}$$

$a_0 = 0$   
 $c_n = 0$

$$C_i^* = \begin{cases} \frac{c_i}{b_i} & i = 0 \\ \frac{c_i}{b_i - C_{i-1}^* a_i} & i = 1, 2, 3, \dots, n-1 \end{cases}$$

$$D_i^* = \begin{cases} \frac{d_i}{b_i} & i = 0 \\ \frac{d_i - D_{i-1}^* a_i}{b_i - C_{i-1}^* a_i} & i = 1, 2, 3, \dots, n \end{cases}$$

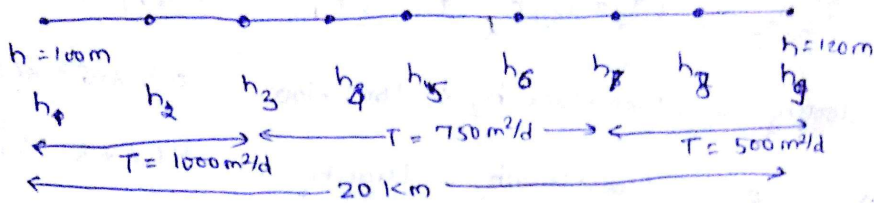
$$x_n = D_n^*$$

$$x_i = D_i^* - C_i^* x_{i+1} \quad i = n-1, n-2, \dots, 0$$

Name - Avinash Jain

Tutorial - 5, CE-423 (Groundwater Engineering)

① Confined aquifer



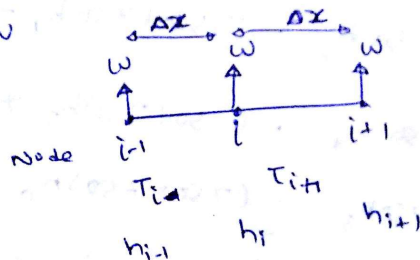
Governing equation

(one-dimensional)

$$\frac{\partial}{\partial x} \left( T \frac{\partial h}{\partial x} \right) - W = S \frac{\partial h}{\partial t}$$

at steady state  $\frac{\partial h}{\partial t} = 0$

$$\Rightarrow T \frac{\partial^2 h}{\partial x^2} = W$$



$$\left( \frac{\partial h}{\partial x} \right)_i = \frac{h_{i+1} - h_{i-1}}{2\Delta x}$$

$$\left( \frac{\partial^2 h}{\partial x^2} \right)_i = \frac{h_{i-1} - 2h_i + h_{i+1}}{(\Delta x)^2}$$

$$\Rightarrow T_i \left[ \frac{h_{i-1} - 2h_i + h_{i+1}}{(\Delta x)^2} \right] = W_i$$

equation at node  $i$

average  $T$  at  $i^{\text{th}}$  node (for simplicity)

For node 1

$$T_{1000} \left[ \frac{h_0 - 2h_1 + h_2}{(\Delta x)^2} \right] = W_1$$

$$\frac{\partial}{\partial x} \left( T \frac{\partial h}{\partial x} \right) = \frac{1}{\Delta x} \left[ T_{i+1} \left( \frac{h_{i+1} - h_i}{\Delta x} \right) - T_i \left( \frac{h_i - h_{i-1}}{\Delta x} \right) \right]$$

Governing equation

$$\frac{\partial}{\partial x} \left( T \frac{\partial h}{\partial x} \right) = W$$

$$\Rightarrow \frac{1}{\Delta x} \left[ T_{i+1} \left( \frac{h_{i+1}}{\Delta x} \right) - \left( \frac{T_j + T_{i+1}}{\Delta x} \right) h_i + \left( \frac{T_i}{\Delta x} \right) h_{i-1} \right] = W$$



$$\frac{1}{(\Delta x)^2} [T_{i+1} h_{i+1} - (T_i + T_{i+1}) h_i + T_i h_{i-1}] = w(\Delta x)^2$$

for node 1

$$T_3 h_3 - (T_2 + T_3) h_2 + T_2 h_1 = w(\Delta x)^2$$

$$\Rightarrow 1000 h_3 - (1000 + 1000) h_2 + 1000 \times 100 = 0.5 \times 10^3 \times (2500)^2$$

$$\Rightarrow 0 - (1000 + 1000) h_2 + 1000 h_3 = -96875 \rightarrow (1)$$

for node (2)  $T_3 h_2 - (T_3 + T_4) h_3 + T_4 h_4 = w(\Delta x)^2$

$$\Rightarrow 1000 h_2 - (1000 + 750) h_3 + 750 h_4 = 3125 \rightarrow (2)$$

for node (4)  $750 h_3 - (750 + 750) h_4 + 750 h_5 = 3125 \rightarrow (3)$

for node (5)  $750 h_4 - (750 + 750) h_5 + 750 h_6 = 3125 \rightarrow (4)$

for node (6)  $750 h_5 - (750 + 750) h_6 + 750 h_7 = 3125 \rightarrow (5)$

for node (7)  $750 h_6 - (750 + 500) h_7 + 500 h_8 = 3125 \rightarrow (6)$

for node (8)  $500 h_7 - (500 + 500) h_8 + 500 h_9 = 3125 \rightarrow (7)$

$$\begin{bmatrix} -2000 & 1000 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1000 & -1750 & 750 & 0 & 0 & 0 & 0 & 0 \\ 0 & 750 & -1500 & 750 & 0 & 0 & 0 & 0 \\ 0 & 0 & 750 & -1500 & 750 & 0 & 0 & 0 \\ 0 & 0 & 0 & 750 & -1500 & 750 & 0 & 0 \\ 0 & 0 & 0 & 0 & 750 & -1500 & 500 & 0 \\ 0 & 0 & 0 & 0 & 0 & 500 & -1000 & 0 \end{bmatrix} \begin{bmatrix} h_2 \\ h_3 \\ h_4 \\ h_5 \\ h_6 \\ h_7 \\ h_8 \end{bmatrix} = \begin{bmatrix} -96875 \\ 3125 \\ 3125 \\ 3125 \\ 3125 \\ 3125 \\ 3125 \\ -56875 \end{bmatrix}$$

$$AH = D$$

$$A = LU$$

$$A = \begin{bmatrix} b_1 & c_1 & 0 & 0 & 0 & 0 & 0 \\ a_2 & b_2 & c_2 & 0 & 0 & 0 & 0 \\ 0 & a_3 & b_3 & c_3 & 0 & 0 & 0 \\ 0 & 0 & a_4 & b_4 & c_4 & 0 & 0 \\ 0 & 0 & 0 & a_5 & b_5 & c_5 & 0 \\ 0 & 0 & 0 & 0 & a_6 & b_6 & c_6 \\ 0 & 0 & 0 & 0 & 0 & a_7 & b_7 \end{bmatrix}$$

$$\alpha_1 = -2000 \quad ; \quad \beta_1 = \frac{c_1}{\alpha_1} \Rightarrow \frac{1000}{-2000} \Rightarrow -0.5$$

$$\alpha_i = b_i - a_i \beta_{i-1}$$

$$\alpha_i = b_i - a_i \frac{c_{i-1}}{\alpha_{i-1}}$$

$$\begin{aligned} \alpha_2 &= b_2 - a_2 \frac{c_1}{\alpha_1} \\ &= -1750 - (1000)(-0.5) \\ &\Rightarrow -1250 \end{aligned}$$

$$\beta_2 = \frac{c_2}{\alpha_2} \Rightarrow \frac{750}{-1250} \Rightarrow -0.6$$

$$\begin{aligned} \alpha_3 &= b_3 - a_3 \beta_2 \\ &\Rightarrow -1500 - 750(-0.6) \\ &\Rightarrow -1050 \end{aligned}$$

$$\beta_3 = \frac{c_3}{\alpha_3} \Rightarrow \frac{750}{-1050} \Rightarrow -0.714$$

$$\begin{aligned} \alpha_4 &= b_4 - a_4 \beta_3 \\ &\Rightarrow -1500 - 750(-0.714) \\ &= -964.285 \end{aligned}$$

$$\beta_4 = \frac{c_4}{\alpha_4} \Rightarrow -0.778$$

$$\begin{aligned} \alpha_5 &= b_5 - a_5 \beta_4 \\ &= -1500 - 750(-0.778) \\ &\Rightarrow -916.667 \end{aligned}$$

$$\beta_5 = \frac{c_5}{\alpha_5} \Rightarrow -0.818$$

$$\begin{aligned} \alpha_6 &= b_6 - a_6 \beta_5 \\ &= -1250 - 750(-0.818) \\ &= -636.363 \end{aligned}$$

$$\beta_6 = \frac{c_6}{\alpha_6} \Rightarrow -0.785$$

$$\begin{aligned} \alpha_7 &= b_7 - a_7 \beta_6 \\ &\Rightarrow -1000 - 500(-0.785) \\ &\Rightarrow -607.142 \end{aligned}$$

$$\beta_7 = \frac{c_7}{\alpha_7} \Rightarrow -0.785$$

$$AH = D$$

$$\Rightarrow LUH = \hat{D}$$

$$UH = y ; H = U^{-1}y$$

$$Ly = D ; y = L^{-1}D$$

$$LU = \begin{bmatrix} \alpha_1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & \alpha_2 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \alpha_3 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \alpha_4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \alpha_5 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & \alpha_6 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \alpha_7 \end{bmatrix} \begin{bmatrix} 1 & \beta_1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & \beta_2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & \beta_3 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & \beta_4 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & \beta_5 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & \beta_6 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

L U

Now,  $Ly = D$

$$\begin{bmatrix} -2000 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1000 & -1250 & 0 & 0 & 0 & 0 & 0 \\ 0 & 750 & -1050 & 0 & 0 & 0 & 0 \\ 0 & 0 & 750 & -964.28 & 0 & 0 & 0 \\ 0 & 0 & 0 & 750 & -964.28 & 0 & 0 \\ 0 & 0 & 0 & 0 & 750 & -636.36 & 0 \\ 0 & 0 & 0 & 0 & 0 & 500 & -607.14 \end{bmatrix}$$

$$\begin{bmatrix} -2000 & 0 & 0 & 0 & 0 & 0 & 0 \\ 1000 & -1250 & 0 & 0 & 0 & 0 & 0 \\ 0 & 750 & -1050 & 0 & 0 & 0 & 0 \\ 0 & 0 & 750 & -964.28 & 0 & 0 & 0 \\ 0 & 0 & 0 & 750 & -916.67 & 0 & 0 \\ 0 & 0 & 0 & 0 & 750 & -636.36 & 0 \\ 0 & 0 & 0 & 0 & 0 & 500 & -607.14 \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \\ y_3 \\ y_4 \\ y_5 \\ y_6 \\ y_7 \end{bmatrix} = \begin{bmatrix} -96875 \\ 3125 \\ 3125 \\ 3125 \\ 3125 \\ 3125 \\ -56875 \end{bmatrix} \begin{matrix} D_1 \\ D_2 \\ D_3 \\ D_4 \\ D_5 \\ D_6 \\ D_7 \end{matrix}$$

$$y_1 = \frac{D_1}{\alpha_1} = \frac{-96875}{-2000} = 48.4375$$

$$y_2 = \frac{\alpha_1 D_2 - \alpha_2 D_1}{\alpha_1 \alpha_2}$$

$$y_i = \frac{D_i - \alpha_i y_{i-1}}{\alpha_i} \quad i \in (2, 7)$$



$$y_2 = \frac{3125 - 1000 \times 48.4375}{-1250} = 36.25$$

$$y_3 = \frac{D_3 - a_{32}y_2}{\alpha_3} = \frac{3125 - 750 \times 36.25}{-1050} = 22.9167$$

$$y_4 = \frac{D_4 - a_{43}y_3}{\alpha_4} = \frac{3125 - 750 \times 22.9167}{-964.2857} = 14.583$$

$$y_5 = \frac{D_5 - a_{54}y_4}{\alpha_5} = \frac{3125 - 750 \times 14.583}{-916.67} = 8.5224$$

$$y_6 = \frac{3125 - 750 \times 8.5224}{-636.636} = 5.1313$$

$$y_7 = \frac{-56875 - 500 \times 5.1313}{-607.1424} = 97.902$$

Now,  $UH = y$

$$\begin{bmatrix} 1 & -0.5 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & -0.6 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & -0.714 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & -0.777 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & -0.818 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & -0.785 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} h_2 \\ h_3 \\ h_4 \\ h_5 \\ h_6 \\ h_7 \\ h_8 \end{bmatrix} = \begin{bmatrix} 48.4375 \\ 36.25 \\ 22.9167 \\ 14.583 \\ 8.5224 \\ 5.1313 \\ 97.902 \end{bmatrix}$$

So, We have  $h_8 = 97.902 \text{ m}$

$$h_7 - 0.785h_8 = 5.1313$$

$$h_7 = 5.1313 + 0.785 \times 97.902 \Rightarrow 81.9846 \text{ m}$$

$$\Rightarrow h_6 - 0.818h_7 = 8.5224$$

$$h_6 = 0.818 \times 81.9846 + 8.5224 \Rightarrow 75.5854 \text{ m}$$

$$h_5 = 14.583 + 0.777 \times 75.5854 = 73.3128 \text{ m}$$

$$h_4 = 22.9167 + 0.710 \times 73.3128 = 75.262 \text{ m}$$

$$h_3 = 36.25 + 0.6 \times 75.262 = 81.4672 \text{ m}$$

$$h_2 = 48.4375 + 0.5 \times 81.4672 = 89.1411 \text{ m}$$

2

② Assume uniform transmissivity =  $750 \text{ m}^2/\text{day}$  on all nodes for 1D, steady state flow in confined aquifer

$$T \frac{\partial^2 h}{\partial x^2} = W$$

$$\frac{\partial h}{\partial x} = \frac{W}{T} x + C_1$$

$$h = \frac{Wx^2}{2T} + C_1 x + C_2$$

$$\text{at } x=0, \quad h=100 \text{ m}$$

$$\Rightarrow C_2 = 100$$

$$\text{at } x=20000, \quad h=120 \text{ m}$$

$$120 = \frac{5 \times 10^{-4}}{2 \times 750} (20000)^2 + C_1 (20000) + 100$$

$$\Rightarrow C_1 = -5.667 \times 10^{-3}$$

$$\text{So, } h = \frac{5 \times 10^{-4}}{2 \times 750} x^2 - 5.667 \times 10^{-3} x + 100$$

$$h = 3.333 \times 10^{-7} x^2 - 5.667 \times 10^{-3} x + 100$$

80,

 $x$  (m)

Head Profile

Along the length

①

 $h$  (m)  
(uniform T) $h$  (m)  
(non uniform T)

0	100	100
2500	87.91	89.14
5000	79.99	81.40
7500	76.24	75.26
10000	76.66	73.31
12500	81.24	75.58
15000	89.98	81.98
17500	102.9	97.90
20000	120	120

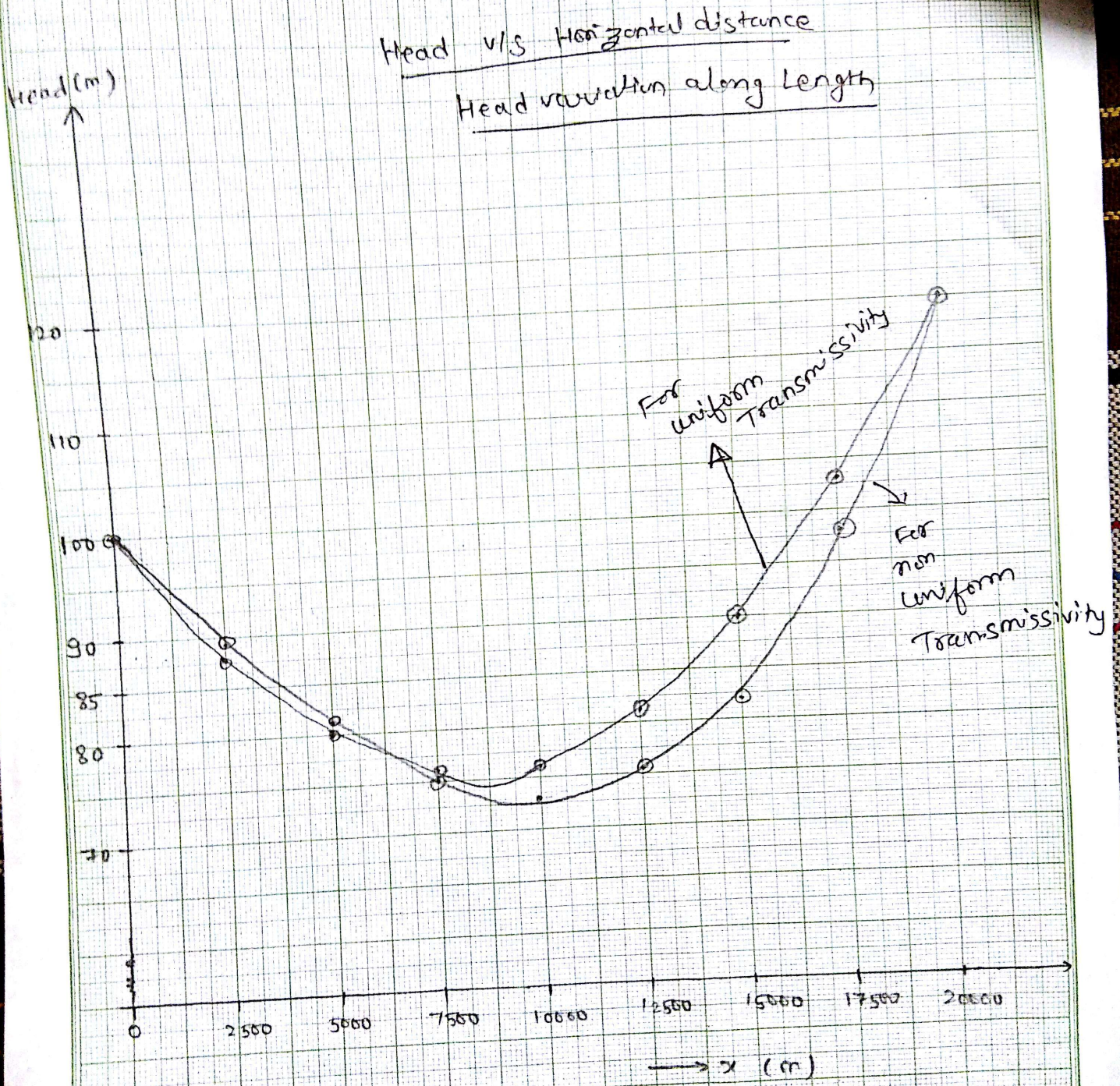


Name \_\_\_\_\_

Class \_\_\_\_\_

Section \_\_\_\_\_

Roll No. \_\_\_\_\_



Measurement Chart of :

Remarks :

Signature :

T. V. H. I. / hi /